

HAWC2 Course

Lesson 3: Control interface

$$f(x+\Delta x) = \sum_{i=0}^{\infty} \frac{(\Delta x)^i}{i!} f^{(i)}(x) \quad \int_a^b \epsilon \Theta + \Omega \int \delta e^{i\pi} = \{2.7182818284\}$$

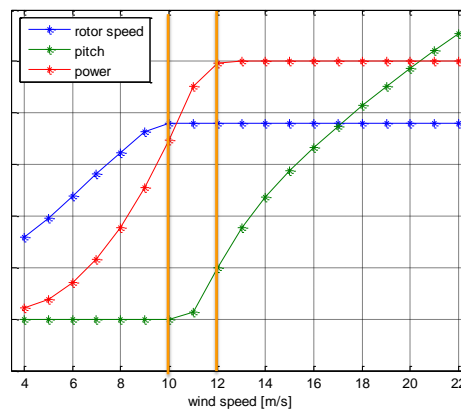
Risø DTU
National Laboratory for Sustainable Energy

Pitch control with variable speed

Objectives: Optimize power production below rated wsp, limit power and loads at high wsp.

Region

1. Variable speed, opt. power tracking.
2. Constant speed.
3. Power limitation

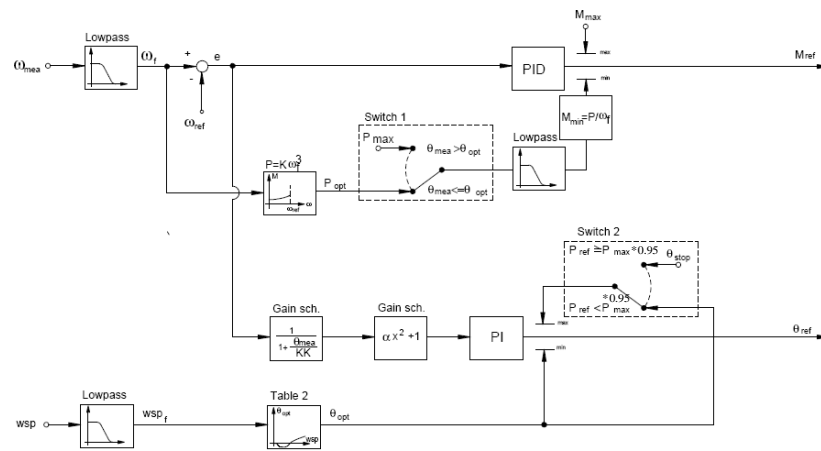


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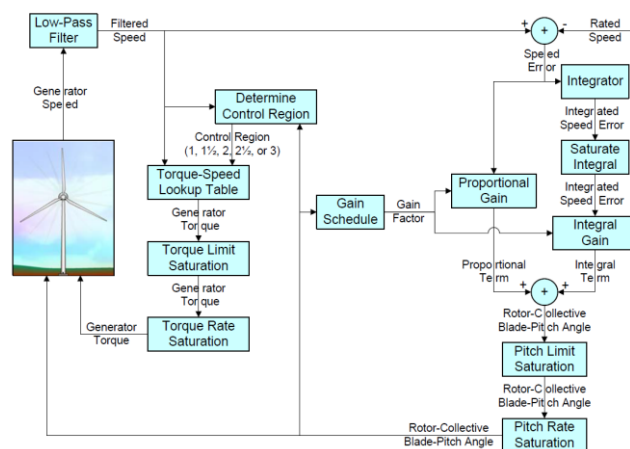
Control diagram Old Risø controller



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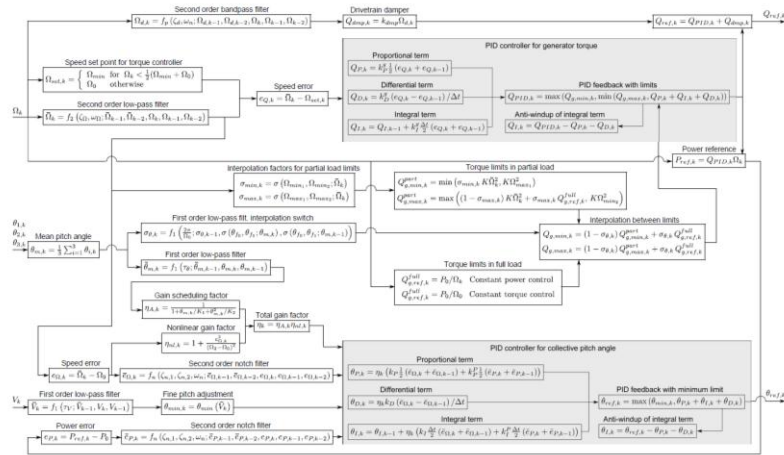
Control

Control diagram NREL 5MW Controller

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Control

Control Diagram DTU Wind Energy Basic Controller

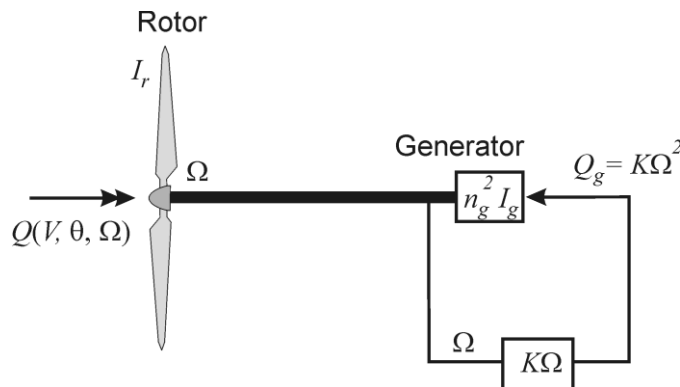


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Region 1: Optimal C_p tracking (1)

Strategy: Keep pitch angle at optimum and use generator torque to obtain optimal tip speed ratio in a torque equilibrium



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Region 1: Optimal Cp tracking (2)

Optimal aerodynamic power and torque

$$P_{\text{aero}} = \frac{1}{2} \rho A V^3 C_p(\theta_{\text{opt}}, \lambda_{\text{opt}}) \Rightarrow Q_{\text{aero}} = \underbrace{\frac{\frac{1}{2} \rho A R^3 C_p(\theta_{\text{opt}}, \lambda_{\text{opt}})}{\lambda_{\text{opt}}^3}}_{K_{\text{no loss}}} \Omega^2$$

Power equilibrium with losses described by efficiency η

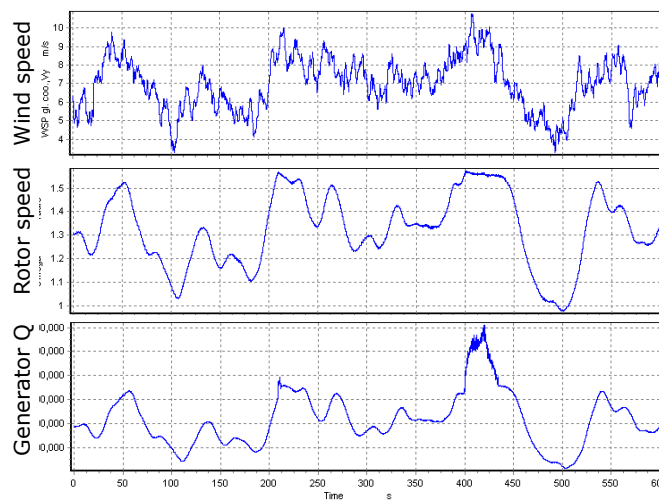
$$P_{\text{elec}} = Q_g \Omega = P_{\text{aero}} - P_{\text{loss}} = \eta P_{\text{aero}} = \eta K_{\text{no loss}} \Omega^3$$

Torque equilibrium

$$Q_g = \eta K_{\text{no loss}} \Omega^2 = K \Omega^2 \text{ where } K = \eta \frac{\frac{1}{2} \rho A R^3 C_p(\theta_{\text{opt}}, \lambda_{\text{opt}})}{\lambda_{\text{opt}}^3}$$

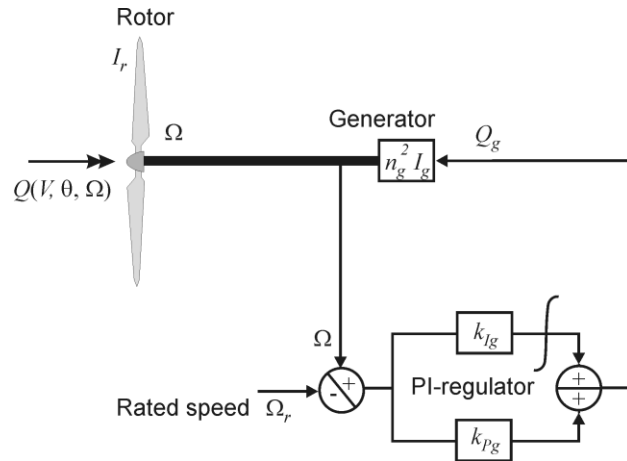
Region 1: Optimal Cp tracking (3)

Example:



Region 2: Speed regulation

Strategy: Keep pitch angle at optimum and use generator torque to regulate rotor speed to the rated speed



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Region 2: Speed regulation (2)

Nonlinear equation of drivetrain motion

$$(I_r + n_g^2 I_g) \dot{\Omega} = Q(V, \Omega, \theta) - \frac{1}{\eta} Q_g$$

PI feedback from speed error to generator torque

$$\begin{aligned} \Delta Q_g &= k_{Pg} (\Omega - \Omega_r) + k_{Ig} \int_0^t (\Omega - \Omega_r) dt \\ &= k_{Pg} \dot{\phi} + k_{Ig} \phi, \text{ where } \dot{\phi} = \frac{d\phi}{dt} = \Omega - \Omega_r \end{aligned}$$

Linear closed-loop equation for small drivetrain motion about $\Omega = \Omega_r + \phi$

$$\underbrace{(I_r + n_g^2 I_g)}_{\text{mass}} \ddot{\phi} + \underbrace{\left(\frac{1}{\eta} k_{Pg} - \frac{\partial Q}{\partial \Omega} \bigg|_0 \right)}_{\text{damping}} \dot{\phi} + \underbrace{\frac{1}{\eta} k_{Ig}}_{\text{stiffness}} \phi = 0$$

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Region 2: Speed regulation (3)

Linear closed-loop equation for small drivetrain motion about $\Omega = \Omega_r + \dot{\phi}$

$$\underbrace{(I_r + n_g^2 I_g)}_{\text{mass}} \ddot{\phi} + \underbrace{\frac{1}{\eta} k_{Pg}}_{\text{damping}} \dot{\phi} + \underbrace{\frac{1}{\eta} k_{Ig}}_{\text{stiffness}} \phi = 0$$

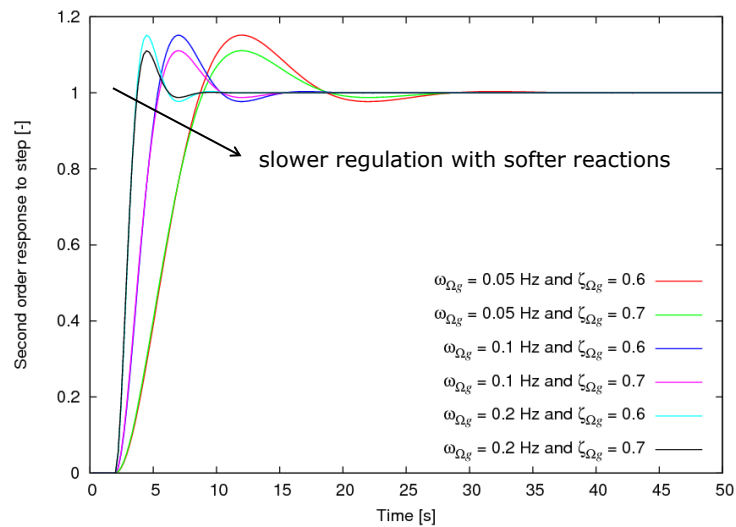
Tuning by placement of closed-loop drivetrain poles/eigenvalues

$$\begin{aligned} k_{Pg} &= 2 \eta \zeta_{\Omega_g} \omega_{\Omega_g} (I_r + n_g^2 I_g) \\ k_{Ig} &= \eta \omega_{\Omega_g}^2 (I_r + n_g^2 I_g) \end{aligned} \Rightarrow \lambda = -\zeta_{\Omega_g} \omega_{\Omega_g} \pm i \omega_{\Omega_g} \sqrt{1 - \zeta_{\Omega_g}^2}$$

Rule of thumb:

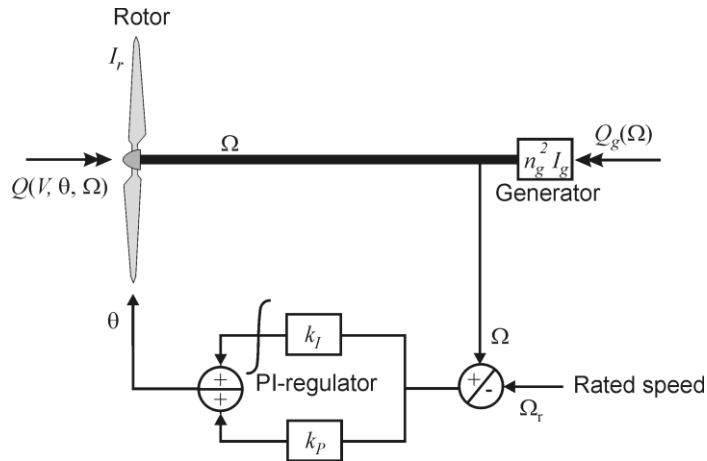
$$\omega_{\Omega_g} = 0.1 \text{ Hz and } \zeta_{\Omega_g} \in [0.6 : 0.7]$$

Region 2: Speed regulation (4)



Region 3: Power and speed regulation

Strategy: Regulate rotor speed by pitching and use generator torque to regulate power (either as constant power, or constant torque)



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Region 3: Power and speed regulation (2)

Nonlinear equation of drivetrain motion

$$(I_r + n_g^2 I_g) \dot{\Omega} = Q(V, \Omega, \theta) - \frac{1}{\eta} Q_g(\Omega)$$

Generator model

$$Q_g(\Omega) = \begin{cases} \frac{P_r}{\Omega_r} & \text{DFIG with ideal constant torque control} \\ \frac{P_r}{\Omega} & \text{DFIG with ideal constant power control} \end{cases}$$

PI feedback from speed error to pitch angle

$$\begin{aligned} \theta &= k_P (\Omega - \Omega_r) + k_I \int_0^t (\Omega - \Omega_r) dt \\ &= k_P \dot{\phi} + k_I \phi, \text{ where } \dot{\phi} = \frac{d\phi}{dt} = \Omega - \Omega_r \end{aligned}$$

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Region 3: Power and speed regulation (3)

Linear closed-loop equation for small drivetrain motion about $\Omega = \Omega_r + \dot{\phi}$

$$\underbrace{(I_r + n_g^2 I_g)}_{\text{mass}} \ddot{\phi} + \underbrace{\left(\frac{1}{\eta} \frac{\partial Q_g}{\partial \Omega} \bigg|_0 - \frac{\partial Q_g}{\partial \Omega} \bigg|_0 - \frac{\partial Q}{\partial \theta} \bigg|_0 k_P \right)}_{\text{damping}} \dot{\phi} - \underbrace{\frac{\partial Q}{\partial \theta} \bigg|_0 k_I}_{\text{stiffness}} \phi = 0$$

Tuning by placement of closed-loop drivetrain pole $\lambda = -\zeta_\Omega \omega_\Omega \pm i \omega_\Omega \sqrt{1 - \zeta_\Omega^2}$

$$k_P = \frac{2 \zeta_\Omega \omega_\Omega (I_r + n_g^2 I_g) - \frac{1}{\eta} \frac{\partial Q_g}{\partial \Omega} \bigg|_0}{-\frac{\partial Q}{\partial \theta} \bigg|_0} \quad \text{where} \quad \frac{\partial Q_g}{\partial \Omega} \bigg|_0 = \begin{cases} 0 & \text{const. torque} \\ -\frac{P_r}{\Omega_r^2} & \text{const. power} \end{cases}$$

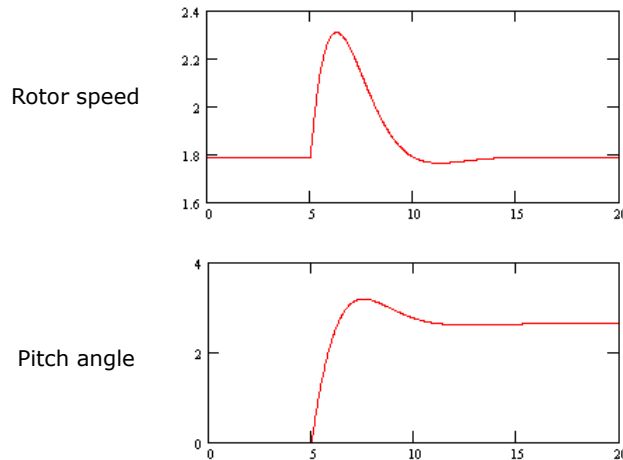
$$k_I = \frac{\omega_\Omega^2 (I_r + n_g^2 I_g)}{-\frac{\partial Q}{\partial \theta} \bigg|_0}$$

Rule of thumb:

$$\omega_\Omega = 0.1 \text{ Hz and } \zeta_\Omega \in [0.6 : 0.7]$$

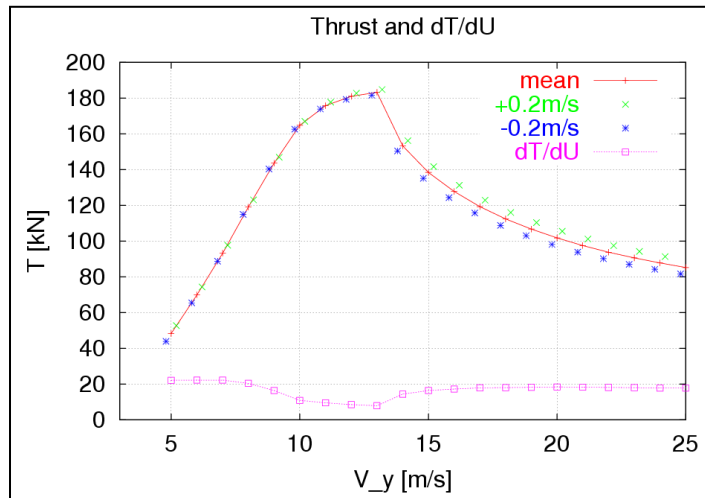
Region 3: Power and speed regulation (4)

Step change in external torque



Region 3: Power and speed regulation (5)

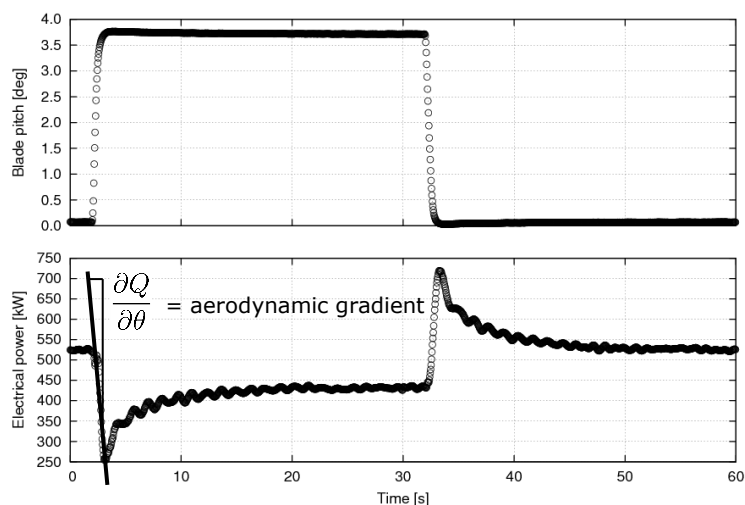
Why is the control frequency so important?



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Region 3: Power and speed regulation (6)



Measurement from old Tjæreborg turbine (Øye, 1991)

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Region 3: Power and speed regulation (7)

Aerodynamic gradient assuming constant induced velocities (frozen wake)

$$\frac{\partial Q}{\partial \theta} = \frac{1}{2} \rho B \int_0^R c(r) U(r)^2 (C'_L(r) \sin \varphi(r) - C'_D(r) \cos \varphi(r)) r dr$$

where

$$C'_L(r) = \left. \frac{dC_L}{d\alpha} \right|_{\alpha=\alpha(r)} \quad c(r) = \text{chord distribution}$$

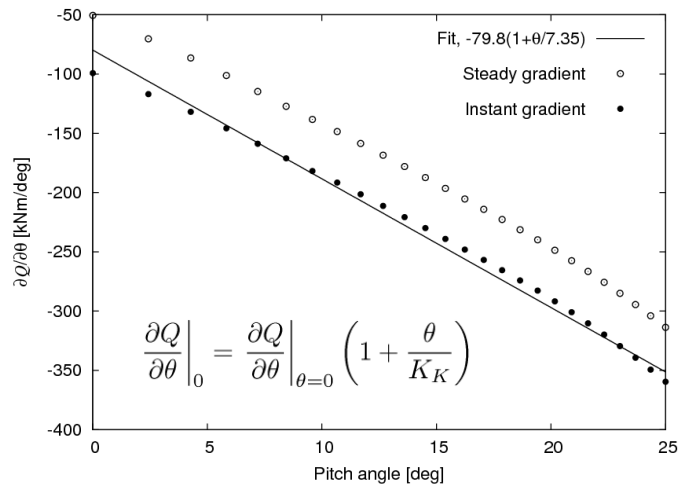
$$C'_D(r) = \left. \frac{dC_D}{d\alpha} \right|_{\alpha=\alpha(r)} \quad U(r) = \text{steady state relative inflow speed}$$

$$\phi(r) = \text{steady state inflow angle}$$

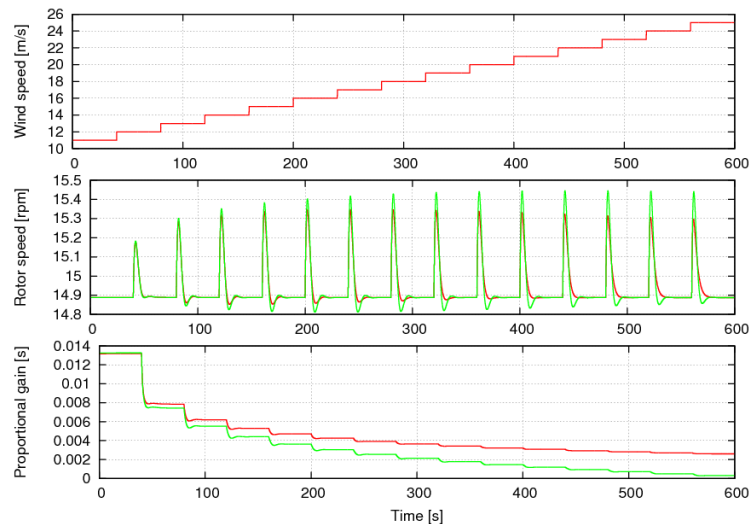
$$\alpha(r) = \text{steady state angle of attack}$$

Region 3: Power and speed regulation (8)

Gain scheduling of aerodynamic gradient



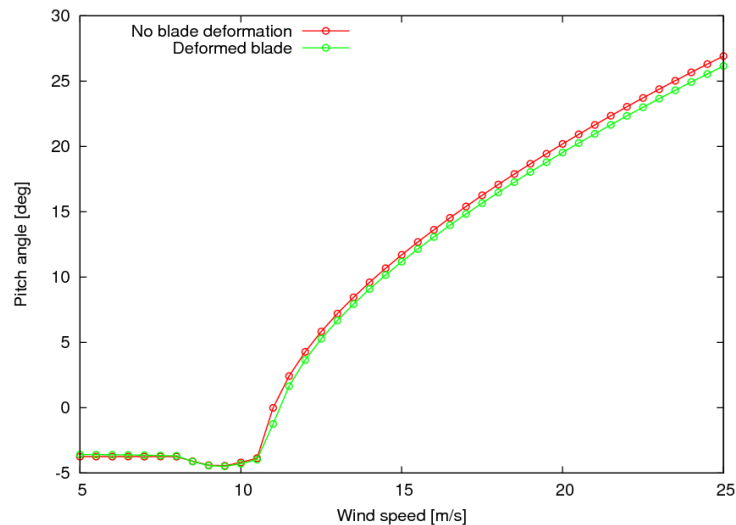
Region 3: Power and speed regulation (9)



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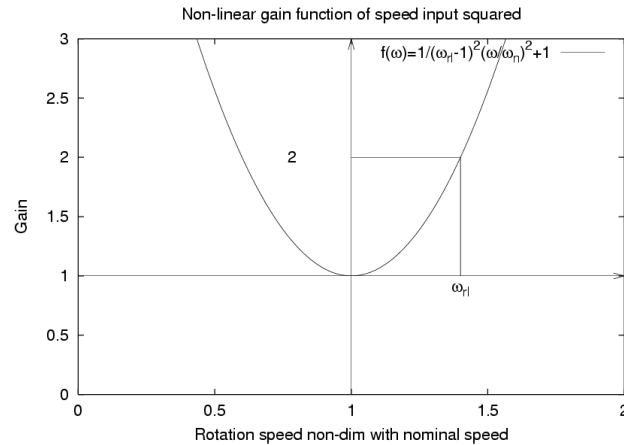
Effect of blade deformations



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Non-linear gain



Gain function used with special low frequent towers (floating turbines etc.)
Parameter is non-dim rotor speed where gain equals 2.0

Tuning of Basic DTU Wind Energy Controller with HAWCStab2

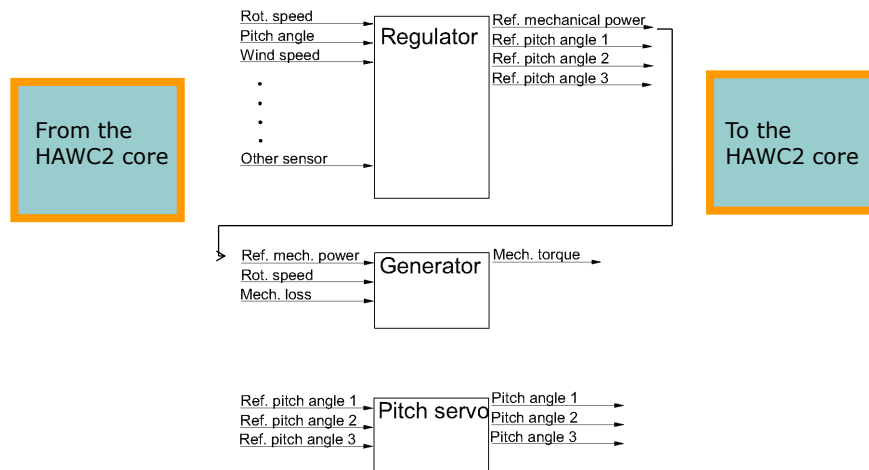
```

begin hawcstab2 ;
begin ground_fixed_substructure ;
  main_body tower ;
  main_body towertop ;
end ground_fixed_substructure ;
begin rotating_axissym_substructure ;
  main_body shaft ;
end rotating_axissym_substructure ;
begin rotating_threebladed_substructure ;
  main_body hub1 ;
  main_body blade1 ;
end rotating_threebladed_substructure ;
...

begin operational_data ;
  windspeed 4.000 25.000 22 ; cut-in, cut-out, points
  genspeed 6.900 12.100 ;
  gearratio 1.000 ;
  minpitch 0.000 ;
  opt_lambda 7.500 ;
  maxpow 5296.610 ;
  prvs_turbine 1 ;
  include_torsiondeform 0 ;
end operational_data ;
begin controller_tuning ;
  partial_load 0.050 0.700 ; fn [hz], zeta [-]
  full_load 0.100 0.700 ; fn [hz], zeta [-]
  gain_scheduling 1 ; 1 linear, 2 quadratic
end controller_tuning ;
end hawcstab2 ;

```

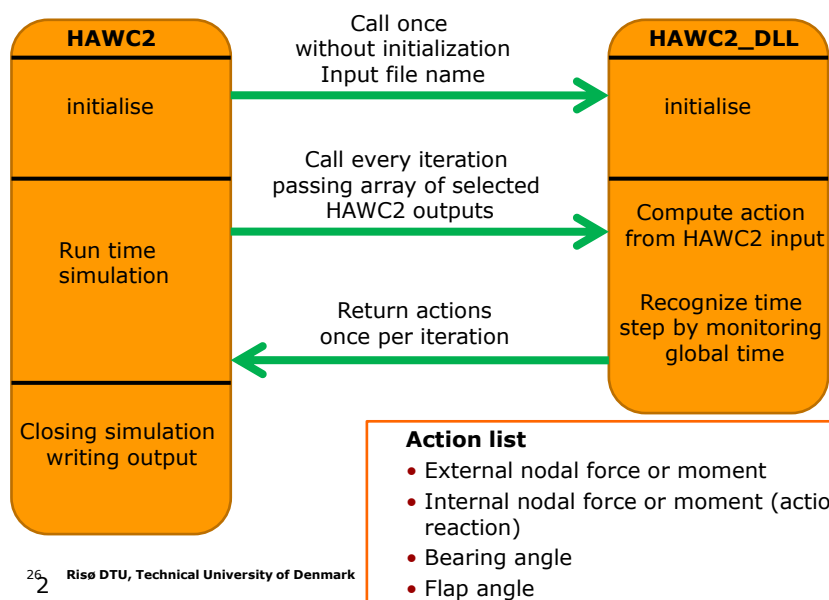
Control through external DLL's



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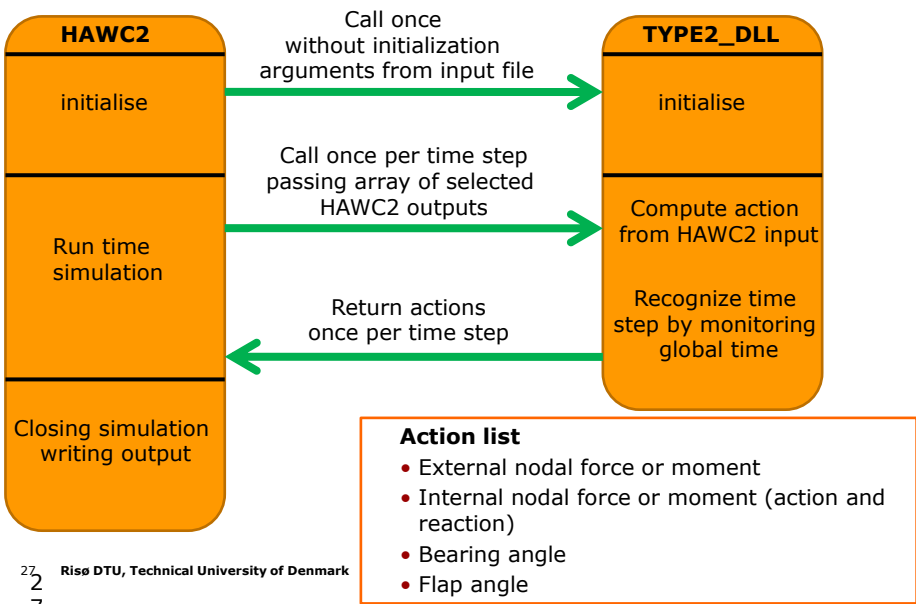
Control

HAWC2_DLL interface



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TYPE2_DLL interface



Coupling of control to HAWC2

```
begin type2_dll;
  name risoe_controller ;
  filename ./control/risoe_controller.dll ;
  dll_subroutine_init init_regulation ;
  dll_subroutine_update update_regulation ;
  arraysizes_init 50 1 ;
  arraysizes_update 8 100 ;
  begin init ;
    ; Overall parameters
    constant 1 5000.0 ; Rated power [kW]
    constant 2 0.7233 ; Minimum rotor speed [rad/s]
    constant 3 1.2671 ; Rated rotor speed [rad/s]
    constant 4 4.598e6 ; Maximum allowable generator torque [Nm]
    constant 5 -1.1 ; Minimum pitch angle, theta_min [deg],
    * * *
    constant 42 0.5 ; PitNonLin1 [rad/s]
  end init ;
;
  begin output ;
    general time ; [s]
    constraint bearing1 shaft_rot 1 only 2 ; Drivetrain speed [rad/s]
    constraint bearing2 pitch1 1 only 1 ; [rad]
    constraint bearing2 pitch2 1 only 1 ; [rad]
    constraint bearing2 pitch3 1 only 1 ; [rad]
    wind free_wind 1 0.0 0.0 -90.0 ; global coords at hub height
    general constant 0.0 ; Pitch rate from external system [rad/s]
  end output ;
end type2_dll;
```

Coupling of simple generator

```
begin type2_dll;
  name generator_servo ;
  filename ./control/generator_servo.dll ;
  dll_subroutine_init init_generator_servo ;
  dll_subroutine_update update_generator_servo ;
  arraysizes_init 6 1 ;
  arraysizes_update 3 6 ;
  begin init ;
    constant 1 20.0 ; Frequency of genertor 2nd order control model [Hz]
    constant 2 0.9 ; Damping ratio of genertor 2nd order control model [-]
    constant 3 4.598e6 ; Maximum allowable LSS torque (pull-out torque) [Nm]
    constant 4 0.944 ; Generator efficiency [-]
    constant 5 1.0 ; Gearratio [-]
  end init ;
;
  begin output;
    general time ; Time [s]
    dll_invec 1 1 ; Electrical torque reference [Nm]
    constraint bearing1 shaft_rot 1 only 2; Generator LSS speed [rad/s]
  end output;
;;
  begin actions;
    mbody moment_int shaft 1 -3 shaft towertop 2 ; Generator LSS torque [Nm]
  end actions;
end type2_dll;
```

Coupling of simple pitch servo

```
begin type2_dll;
  name servo_with_limits ;
  filename ./control/servo_with_limits.dll ;
  dll_subroutine_init init_servo_with_limits ;
  dll_subroutine_update update_servo_with_limits ;
  arraysizes_init 7 1 ;
  arraysizes_update 4 9 ;
  begin init ;
    constant 1 3 ; 1: Number of blades [-]
    constant 2 1.0 ; 2: Filter frequency [Hz]
    constant 3 0.7 ; 3: Filter damping ratio [-]
    constant 4 8.0 ; 4: Max. pitch speed [deg/s]
    constant 5 15.0 ; 5: Max. pitch acceleration [deg/s^2]
    constant 6 -5.0 ; 6: Min. pitch angle [deg]
    constant 7 90.0 ; 7: Max. pitch angle [deg]
  end init ;
  begin output;
    general time ; 1: Time [s]
    dll_invec 1 2 ; 2: Pitch1 demand angle [rad]
    dll_invec 1 3 ; 3: Pitch2 demand angle [rad]
    dll_invec 1 4 ; 4: Pitch3 demand angle [rad]
  end output;
  begin actions;
    constraint bearing2 angle pitch1 ; Angle pitch1 bearing [rad]
    constraint bearing2 angle pitch2 ; Angle pitch2 bearing [rad]
    constraint bearing2 angle pitch3 ; Angle pitch3 bearing [rad]
  end actions;
end type2_dll;
```

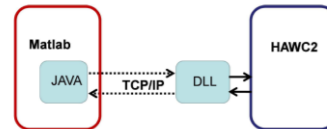
Other dll possibilities

type2_dll

```
begin type2_dll;
  name hss_convert ;
  filename ./hss_convert.dll ;
  dll_subroutine_init 'Initialize' ;
  dll_subroutine_update 'Sensors' ;
  arraysizes_init 3 1 ;
  arraysizes_update 2 2 ;
  begin init ;
    constant 1 2.0 ; number of used sensors
    constant 2 112.43 ; gearbox ratio
    constant 3 112.43 ; gearbox ratio
  end init ;
;
  begin output ;
    constraint bearing1 shaft_rot 2 only 2 ; rotor speed in rpm
    constraint bearing1 shaft_rot 3 only 2 ; rotor speed in rad/s
  end output ;
;
  begin actions;
  ; rotor_speed in rpm*gear_ratio
  ; rotor_speed in rad/s*gear_ratio
  end actions;
end type2_dll;
```

tcp/ip communication with e.g. Matlab or Matlab/Simulink

```
begin hawc_dll;
  filename ./tcpip/TCPserver.dll ;
  dll_subroutine tcpip_delay ;
  init_string 1139 ;
  arraysizes 60 60 ;
  begin output;
    continue_in_file ./htc/tcpiplink_sensors.htc ;
  end output;
;
  begin actions;
  end actions;
end hawc_dll ;
```



Exercise

- Run the file structure_aero_control.htc 600s
- Run the file structure_aero_control_turb.htc 600s