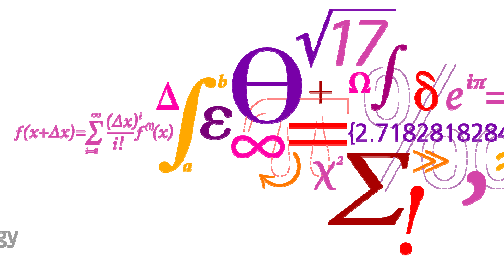


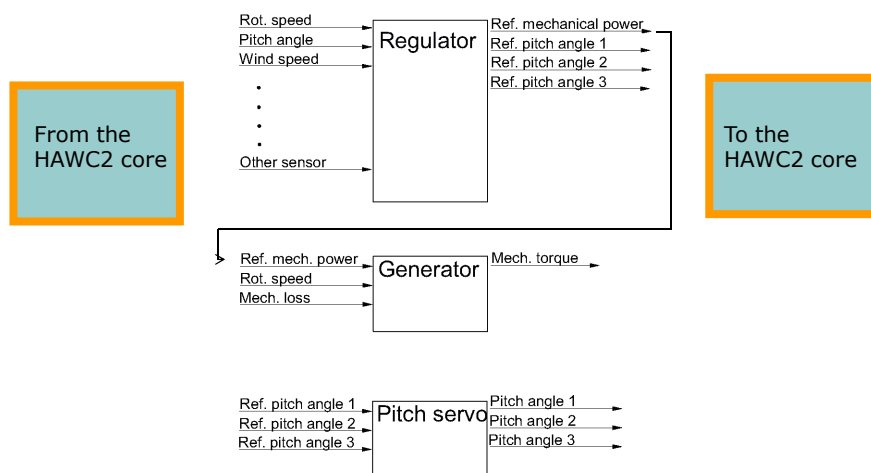
HAWC2 Course

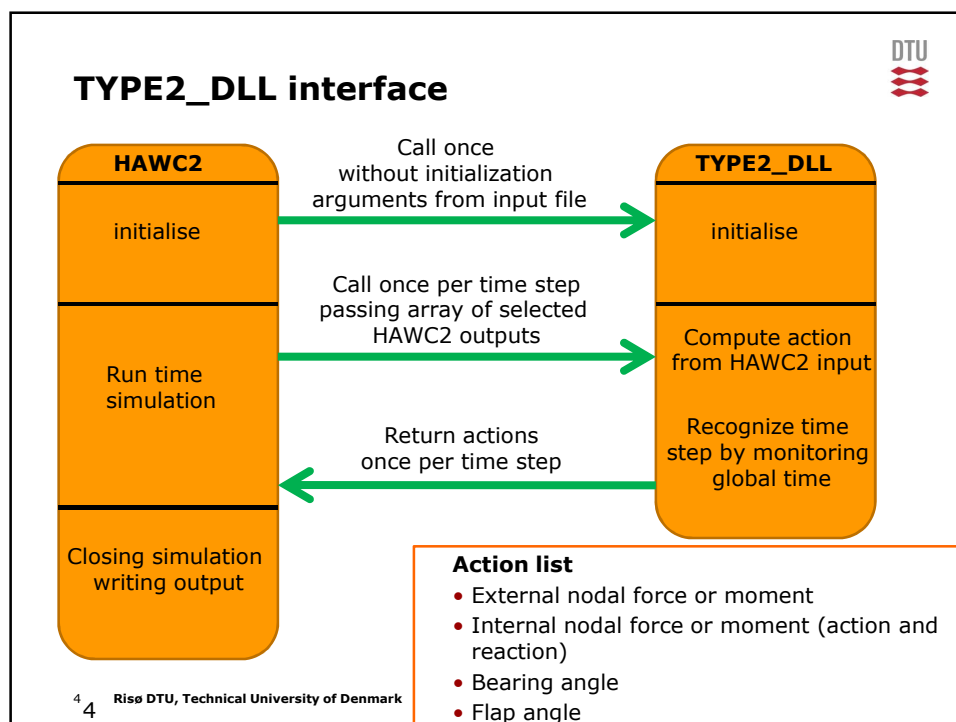
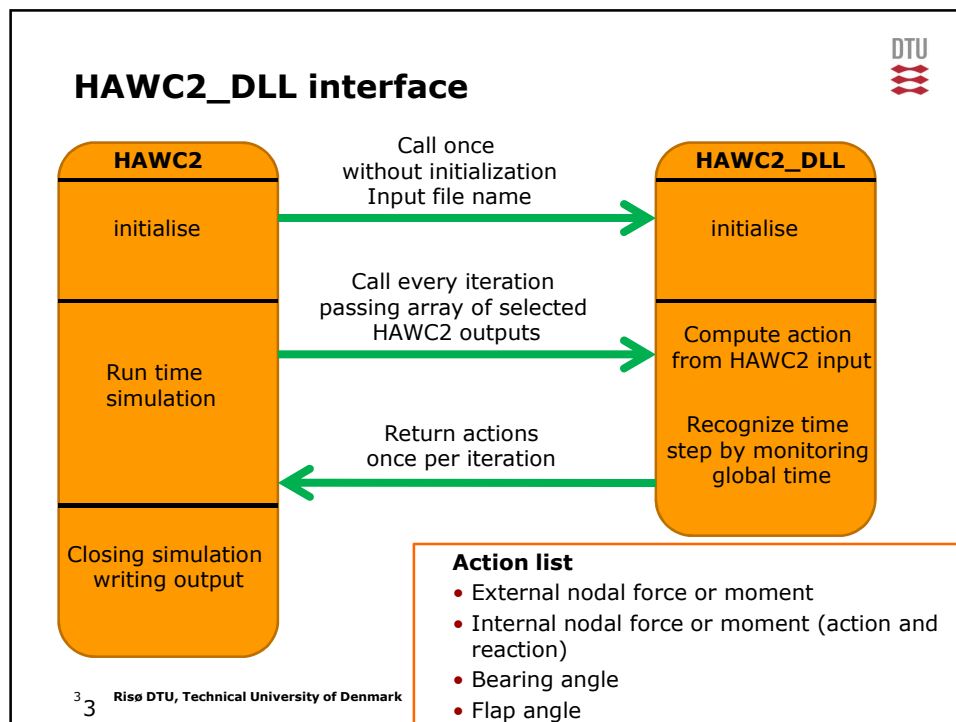
Lesson 3: Control interface



Risø DTU
National Laboratory for Sustainable Energy

Control through external DLL's



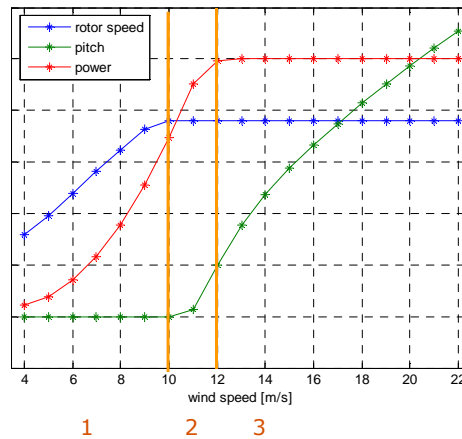


Pitch control with variable speed

Objectives: Optimize power production below rated wsp, limit power and loads at high wsp.

Region

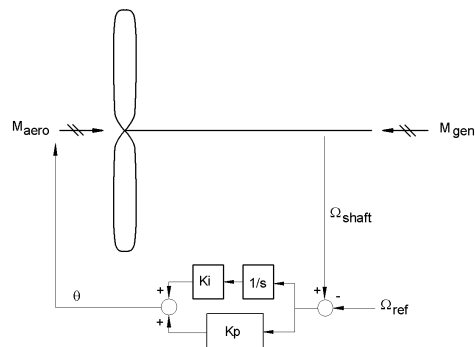
1. Variable speed, opt. power tracking.
2. Constant speed.
3. Power limitation



5 Rise DTU, Technical University of Denmark

Control

Pitch control at high wind speeds



Two different generator strategies:

- Constant power: Good power quality – decent drive train loads
- Constant torque: Good drive train loads – decent power quality

6 Rise DTU, Technical University of Denmark

Control

The derivation of good controller constants



The 1 DOF model

$$I\ddot{\phi} = M_{aero} - M_{gen}$$

The generator torque

$$M_{gen} = M_0 = \frac{P_0}{\Omega_0}$$

"The aerodynamic model"

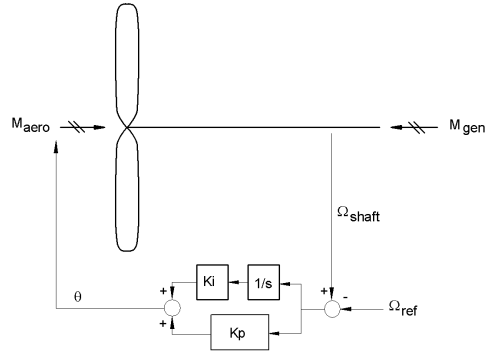
$$M_{aero} = \frac{1}{\Omega} P(V, \theta) \approx \frac{P_0}{\Omega_0} + \frac{1}{\Omega_0} \frac{\partial P}{\partial \theta} (\theta - \theta_0)$$

The controller

$$\theta = \theta_i + \theta_p$$

$$\theta_i = \int K_I (\Omega - \Omega_{ref}) dt = K_I \phi, \quad \Omega_{ref} \equiv \Omega_0$$

$$\theta_p = K_p (\Omega - \Omega_{ref}) = K_p \dot{\phi}$$



Tuning of control parameters



Insertion of the aerodynamic terms

$$I\ddot{\phi} = M_{aero} - M_{gen} = \frac{P_0}{\Omega_0} + \frac{1}{\Omega_0} \frac{\partial P}{\partial \theta} (K_I \phi + K_p \dot{\phi}) - \frac{P_0}{\Omega_0}$$

Rewritten into standard form

$$I\ddot{\phi} + D\dot{\phi} + K\phi = 0$$

$$I = I_{rotor} + n^2 I_{gen} \quad D = -\frac{1}{\Omega_0} \frac{\partial P}{\partial \theta} K_p \quad K = -\frac{1}{\Omega_0} \frac{\partial P}{\partial \theta} K_I$$

Natural frequency and damping

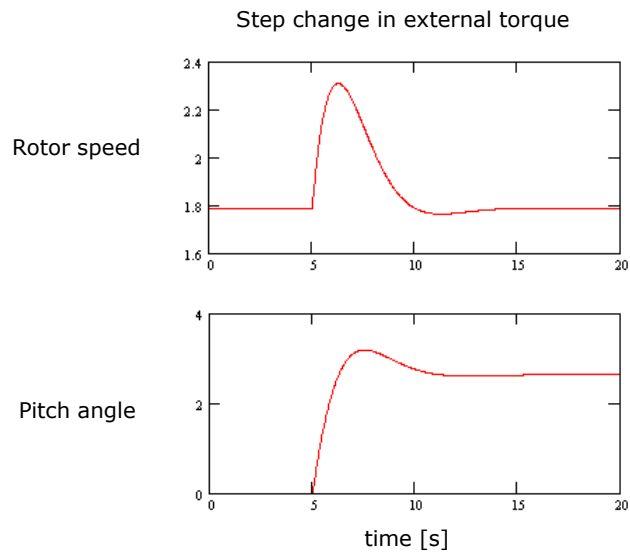
$$\omega_0 = \sqrt{\frac{K}{I}} \quad \zeta = \frac{D}{2I\omega_0} \quad \omega_d = \omega_0 \sqrt{1 - \zeta^2}$$

The constants are now given as function of desired control frequency and damping

$$K_I = \frac{\Omega_0 I \omega_0^2}{-\frac{\partial P}{\partial \theta}} \quad K_p = \frac{2\zeta K_I}{\omega_0}$$

Rule of thumb: $\omega_0 = 0.1 \text{ Hz}$ $\zeta = 0.7$

Response of system



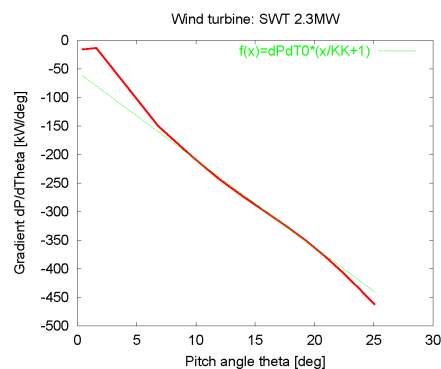
9 Rise DTU, Technical University of Denmark

Control

Gain scheduling



To ensure a similar response at different wind speeds.



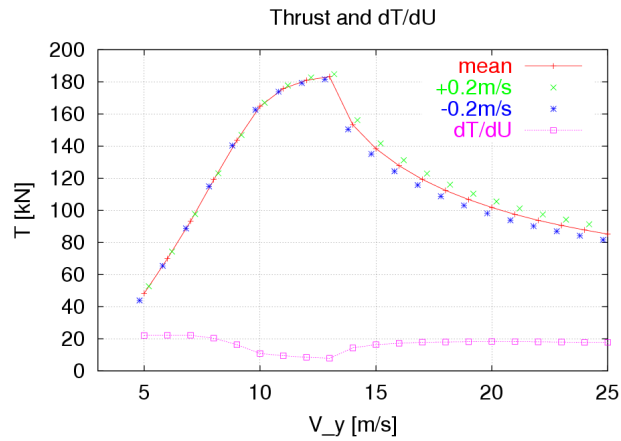
$$G(\theta) = \frac{1}{1 + \frac{\theta}{KK}}$$

KK is the pitch angle
where $\frac{dP}{d\theta}$ is $2 \cdot \frac{dP}{d\theta_0}$

10 Rise DTU, Technical University of Denmark

Control

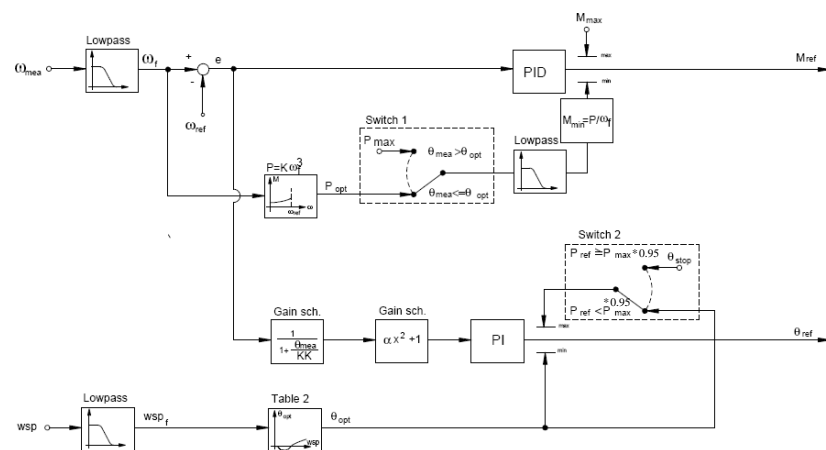
Why is the control frequency so important?



11 Risø DTU, Technical University of Denmark

Control

Control diagram "Risø" controller



12 Risø DTU, Technical University of Denmark

Control

Additional parameters from control file



```

basic_3ba_input_ct10nl - Notepad
File Edit Format View Help
1.267 // omega_ref [rad/s]
0.42 // omega_min [rad/s]
4.38 // kga_set [deg]
10.0 // rel_limit [-]
5000 // pmax (mech) [kw]
1 // const power (1) or constant torque (0)
1431 // Low speed K factor [kNm/(rad/s)^2], torque=K*omega^2, K=0.5*rho*A*Cp*R^3/lambda^3*0.8
0.4 0.7 // f0,ksi [Hz],[-] 2' order filter variables
0.01 // tau_gen [s]
2 // ndata optipitch
0.0 0.0 // wsp [m/s] pitch [deg]
50.0 0.0 // tau_wsp [s]
5.0 // f0 [Hz]
0.1 // pitch stop angle [deg]
88
Ln 15, Col 35

```

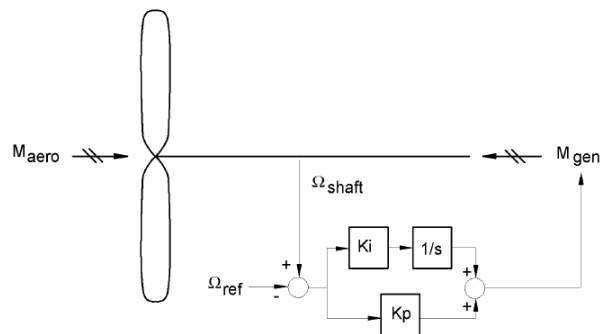
Optimal power tracking at low wind speeds:

$$P = \frac{1}{2} \rho A C_p U^3 = \underbrace{\frac{1}{2} \rho A C_p R^3}_{\text{Constant K}} \omega^3 \quad \lambda = \frac{\omega r}{U}$$

$$T = \frac{P}{\omega} = \frac{1}{2} \rho A C_p R^3 \omega^2$$

In practise K is reduced with app 20% due to mech. losses and to ensure safe operation away from stall.

Operation at intermediate wind speeds

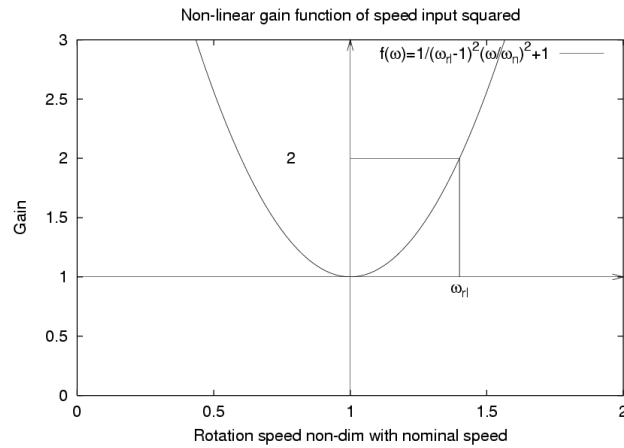


$$M_{aero} = M_{a0}$$

$$M_{gen} = K_{pg} (\Omega - \Omega_{ref}) + \int K_{Ig} (\Omega - \Omega_{ref}) dt = K_{pg} \dot{\varphi} + K_{Ig} \varphi$$

$$K_{Ig} = I \omega_0^2, \quad K_{pg} = \frac{2\zeta K_{Ig}}{\omega_0}$$

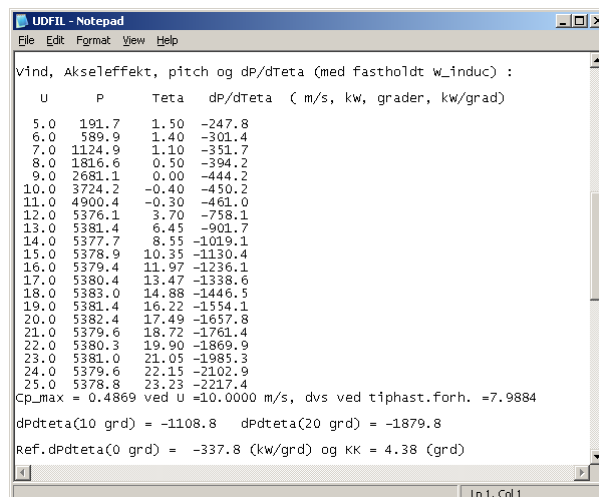
Non-linear gain



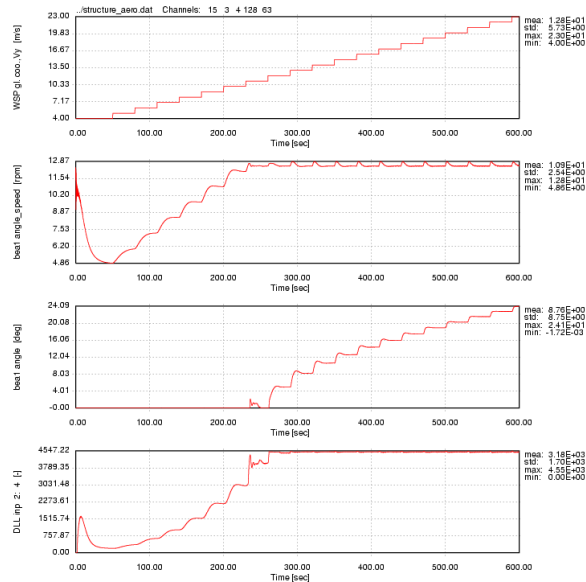
Gain function used with special low frequent towers (floating turbines etc.)

Parameter is non-dim rotor speed where gain equals 2.0

Calculated results from small WT4 BEM code



Response to step change in wind



17 Risø DTU, Technical University of Denmark

Control

Coupling of control to HAWC2



```
begin dll;
  begin hawc_dll;
    filename ./control/basic_3ba-ct10n1.dll ;
    dll_subroutine regulation ;
    arraysizes 25 15 ;
  ;
  ; deltat 0.02;
  begin output;
    general constant 1 ;   inputfile extension           1
    general time ;        2
    constraint bearing1 hub_rot 1 only 2;   speed generator 3
    constraint bearing2 pitch1 1 only 1;    4
    constraint bearing2 pitch2 1 only 1;    5
    constraint bearing2 pitch3 1 only 1;    6
    wind free_wind 1 0.0 0.0 -123.0 ; coordsys (1:glo, 2:ikkerot rotor), 7,8,9
    general constant 2.02 ;   Kp pitch           10
    general constant 0.764 ;  Ki pitch           11
    general constant 0.00 ;   Kd pitch           12
    general constant 2.43E7 ; Kp torque          13
    general constant 1.09E7 ; Ki torque          14
    general constant 0.0 ;    Kd torque          15
    general constant 750 ;    generator stoptime 16
    general constant 0.2 ;    pitch stopdelay    17
    general constant 8 ;      pitch stop velmax  18
    general constant 0 ;      stop type (not used) 19
    general constant -1 ;     cut-in time        20
    general constant 10 ;     pitch stop delay 2 21
    general constant 2 ;      pitch stop velmax 2 22
    general constant 10 ;     pitch velmax runtime 23
  end output;
end dll;
```

18 Risø DTU, Technical University of Denmark

Control

Coupling of simple generator

```
begin hawc_dll;
  filename ./control/basic_3ba_ct10n1.dll ;
  dll_subroutine generator ;
  arraysizes 15 15 ;
;  deltat 0.02 ;
  begin output;
    general time ;
    dll_inpvec 1 1; input t11 h2, dll no 1, plads no 1
    general constant 0.93; Efficiency factor
    constraint bearing1 shaft_rot 1 only 2; speed generator
    general constant 1.0 ;
  end output;
;
  begin actions;
    mbody moment_int shaft 1 -3 shaft tower 10 ; generator torque LSS
  end actions;
end hawc_dll;
```

Coupling of simple pitch servo

```
begin hawc_dll;
  filename ./control/basic_3ba_ct10n1.dll ;
  dll_subroutine pitchservo ;
  arraysizes 15 15 ;
  begin output;
    general time ;
    dll_inpvec 1 2;
    dll_inpvec 1 3;
    dll_inpvec 1 4;
    constraint bearing2 pitch1 1 only 1; 3
    constraint bearing2 pitch2 1 only 1; 4
    constraint bearing2 pitch3 1 only 1; 5
  end output;
;
  begin actions;
    constraint bearing2 angle pitch1;
    constraint bearing2 angle pitch2;
    constraint bearing2 angle pitch3;
  end actions;
end hawc_dll;
end dll;
```

Other dll possibilities

type2_dll

```
begin type2_dll;
  name hss_convert ;
  filename ./hss_convert.dll ;
  dll_subroutine_init 'Initialize' ;
  dll_subroutine_update 'Sensors' ;
  arraysizes_init 3 1 ;
  arraysizes_update 2 2 ;
  begin init ;
    constant 1 2.0 ; number of used sensors
    constant 2 112.43 ; gearbox ratio
    constant 3 112.43 ; gearbox ratio
  end init ;
;
  begin output ;
    constraint bearing1 shaft_rot 2 only 2 ; rotor
    speed in rpm
    constraint bearing1 shaft_rot 3 only 2 ; rotor
    speed in rad/s
  end output ;
;
  begin actions;
    ; rotor_speed in rpm*gear_ratio
    ; rotor_speed in rad/s*gear_ratio
  end actions;
end type2_dll;
```

tcp/ip communication with e.g. Matlab
or Matlab/Simulink

```
begin hawc_dll;
  filename ./tcpip/TCPserver.dll ;
  dll_subroutine tcpip_delay ;
  init_string 1139 ;
  arraysizes 60 60 ;
  begin output;
    continue_in_file ./htc/tcpip_sensors.htc ;
  end output;
;
  begin actions;
  end actions;
end hawc_dll ;
```

